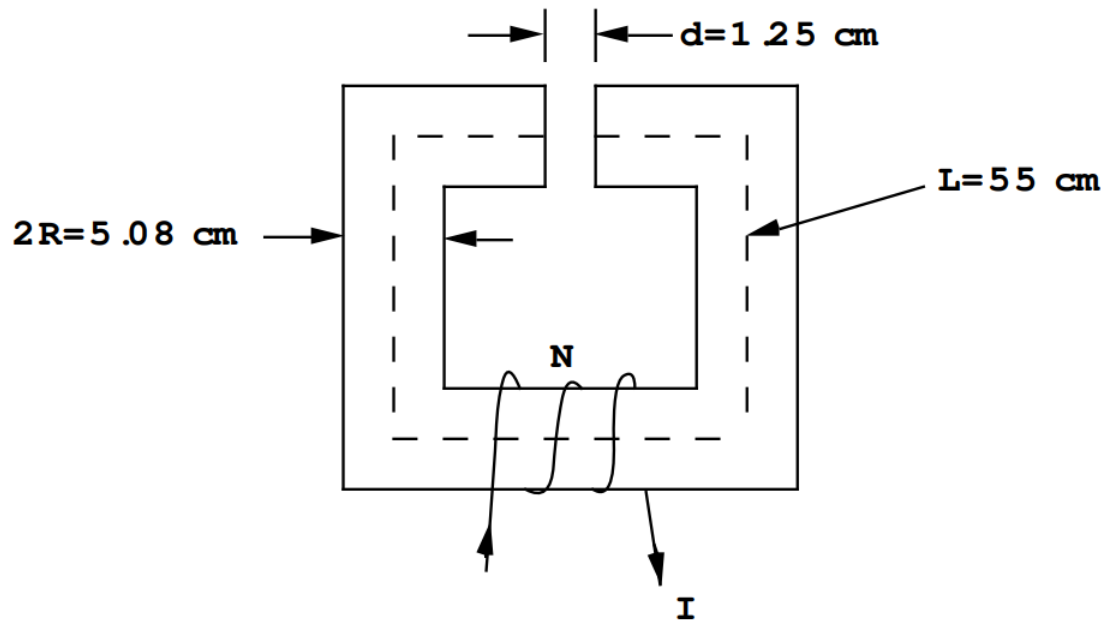


## 13.6: Chapter 6

### Problem (6.1)

An electromagnet is constructed of a soft iron yoke, see the diagram. The yoke radius is  $R = 2.54$  cm, and the gap is  $d = 1.25$  cm. The distance from pole face to pole face along the dotted line is  $L = 55$  cm. The number of turns on the coil is 1000 windings. Estimate the current required to generate a field of 1.0 Teslas at the center of the magnet gap. A field of 1.0 T in the iron yoke corresponds to a field  $H$  of 130 Amps/m.



### Answer (6.1)

$$\oint_C \mathbf{H} \cdot d\mathbf{L} = NI$$

$$\text{Therefore, } 130L + d/\mu_0 = NI.$$

or

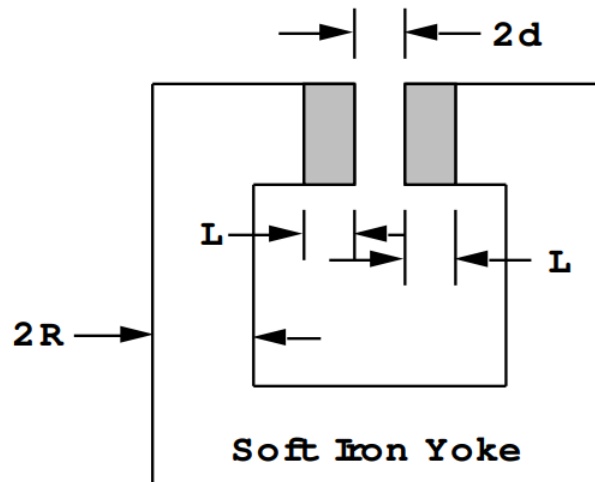
$$(13)(0.55) + (0.0125)/(4\pi \times 10^{-7}) = 10^3 I,$$

and

$$I = 10.0 \text{ Amps.}$$

### Problem (6.2)

Modern permanent magnet materials such as FeNdB can be used to generate substantial magnetic fields. Consider the configuration shown in the diagram where the cross-hatched regions represent FeNdB permanent magnets.



The saturation magnetization density in each magnet is  $M_0 = 0.8 \times 10^6$  Amps/m., ie.  $B = \mu_0 M_0 = 1.01$  Teslas. Let  $R = L = 1.0$  cm., and let  $d = 1/2$  cm.

Calculate the field  $B$  at the midpoint of the gap. The approximate effect of the iron yoke is to make each permanent magnet appear to be infinitely long due to the magnetization induced in the soft iron. In soft iron having a very large permeability the magnetization must be continuous at the iron-magnet interface because a discontinuity in  $\mathbf{M}$  would produce an  $\mathbf{H}$ -field which would produce a large  $\mathbf{M}$  in the iron and as a result  $\mathbf{B}$  would not be continuous.

#### Answer (6.2)

The field generated at the gap center can be approximated using a superposition argument. If there were no gap the field would be that due to an infinitely long solenoid having  $NI = M_0$ , ie.  $B = \mu_0 M_0$ .

The field in the gap,  $B_G$ , plus the field at the center due to a magnetized section  $2d$  long must equal  $\mu_0 M_0$ . A section  $2d$  long possessing a magnetization density  $M_0$  produces a field at its center given by the short solenoid formula  $B_s = \frac{\mu_0 M_0 d}{\sqrt{d^2 + R^2}}$ .

Therefore

$$B_G + B_s = \mu_0 M_0,$$

and

$$B_G = \mu_0 M_0 \left( 1 - \frac{d}{\sqrt{d^2 + R^2}} \right).$$

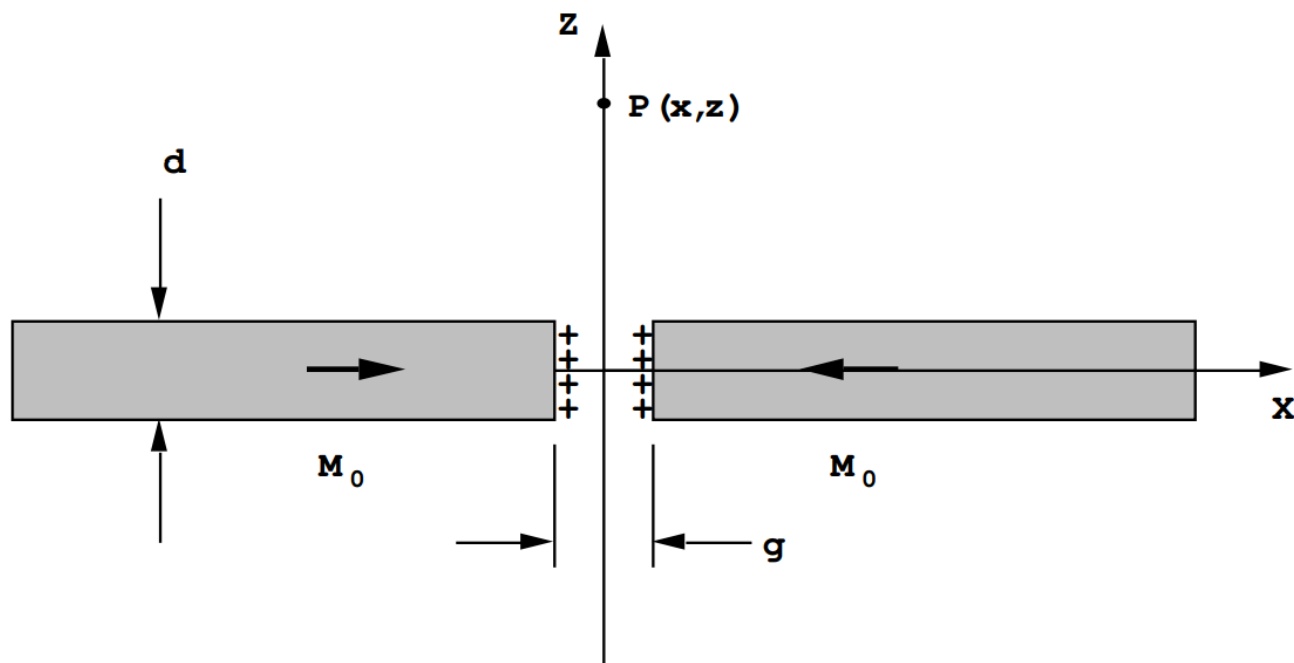
In this case  $d = 1/2$  cm and  $R = 1$  cm, so  $B_G = 0.558$  Teslas.

R. Oldenbourg and W.C. Phillips,

(Rev.Sci.Instrum.57,2362(1986) and 57,3139(1986)), used  $2d = 1.9$  cm and soft iron pole tips tapered to 0.35 cm in diameter to produce a field of 2 Teslas in a 0.2 cm gap.

#### Problem (6.3)

This problem has to do with the fields produced in the region between two magnetized bits on a hard disc, see the figure. The gap is  $g = 10^{-8}$  meters, the thickness is  $d = 10^{-8}$  meters, and the width of each magnetized region is  $w = 0.4 \times 10^{-6}$  meters. the magnetization is  $M_0 = 6.4 \times 10^5$  Amps/m.



The end of each magnetized region bears a surface charge of  $M_0$  per square meter due to the discontinuity in the magnetization density.

Calculate the field at  $P(x,0,z)$  on the centerline of the gap between the two magnetized regions due to the magnetic surface charges.

**Answer (6.3)**

On the centerline  $\mathbf{H}$  has only a  $z$ -component by symmetry.

Let  $\mathbf{r} = (g/2)\mathbf{u}_x + y\mathbf{u}_y + z\mathbf{u}_z$ ,

and  $\mathbf{R} = Z\mathbf{u}_z$ .

The vector from the element of magnetic charge  $dq = dydzM_0$  to the point of observation is  $\rho = \mathbf{R} - \mathbf{r} = -(g/2)\mathbf{u}_x - y\mathbf{u}_y + (Z - z)\mathbf{u}_z$ , and  $|\rho| = \sqrt{(g/2)^2 + y^2 + (Z - z)^2}$ .

For one of the end faces

$$H_z = \frac{M_0}{4\pi} \int_{-d/2}^{d/2} dz (z - z) \int_{-w/2}^{w/2} dy \frac{1}{(y^2 + (g/2)^2 + (Z - z)^2)^{3/2}}.$$

Now

$$\int_{-w/2}^{w/2} \frac{dy}{(y^2 + a^2)^{3/2}} = \frac{w}{a^2 \sqrt{(w/2)^2 + a^2}},$$

therefore

$$H_z = \frac{M_0 w}{4\pi} \int_{-d/2}^{d/2} dz \frac{(Z - z)}{((g/2)^2 + (Z - z)^2) \sqrt{(Z - z)^2 + (g/2)^2 + (w/2)^2}}$$

Let  $v = (Z - z)^2 + (g/2)^2$ , then the integral becomes

$$H_z = \frac{M_0 w}{8\pi} \int_{(Z-d/2)^2 + (g/2)^2}^{(Z+d/2)^2 + (g/2)^2} dv \frac{1}{v \sqrt{v + (w/2)^2}}.$$

This is a standard integral:

$$H_z = \frac{M_0}{2\pi} \left\{ \tanh^{-1} \left[ \frac{2}{w} \sqrt{(w/2)^2 + (g/2)^2 + (Z - d/2)^2} \right] - \tanh^{-1} \left[ \frac{2}{w} \sqrt{(w/2)^2 + (g/2)^2 + (z + d/2)^2} \right] \right\}.$$

(This is for one face of the gap magnetic charge distribution- it must be multiplied by 2 to obtain the total field).

For  $(w/2)=20 \times 10^{-8}$ ,  $(g/2)=(1/2) \times 10^{-8}$ , and  $(d/2)= (g/2)$ , and if  $Z= 1.0 \times 10^{-8}$  meters  $B_z= \mu_0 H_z= 0.206$  Teslas. For the above parameters  $B_z$  is a maximum for  $Z=0.71 \times 10^{-8}$  meters. The maximum value of  $B_z= 0.224$  T. At  $Z=2 \times 10^{-8}$  m the field has dropped to  $B_z= 0.121$  T.

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